

Two-Dimensional Stress Corrosion Cracking Model for Reactor Structural Materials

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Background and Objective

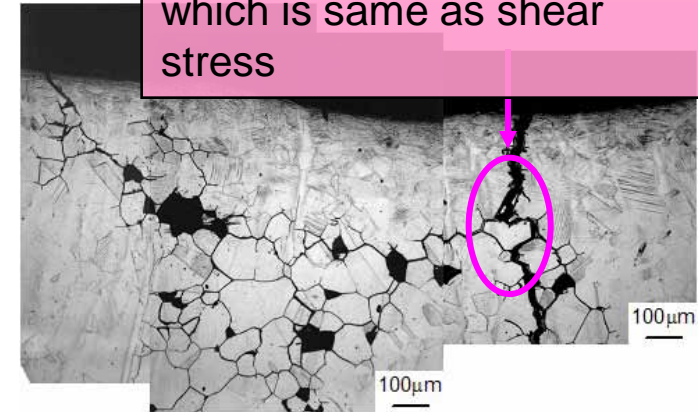
[Background]

Stress corrosion cracking (SCC) is one of the main causes of the trouble in the nuclear power plant.

<SCC model yet proposed>

- rate equation theory
- SCC crack growth model (only vertical stress)

New SCC crack growth model is expected (includes crack branching, corrosion, ...)



SCC crack at core shroud of boiled water reactor

[Objective]

- Development of new Intergranular stress corrosion cracking (IGSCC) growth model
- Determination of the cause of each IGSCC behavior

Several micron-order effects are modeled and crack growth path is obtained

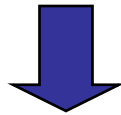
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|--|-------------------------------|--|
| <div style="border-left: 1px solid black; border-right: 1px solid black; border-bottom: 1px solid black; padding: 5px; display: inline-block;"> </div> | Strength of grain boundary | à small fluctuation in strength |
| | Influence of shear stress | à “ net stress ” constructed with vertical and shear stress |
| | degradation of grain boundary | à corrosion of grain boundary |

2-Dimensional SCC Crack Growth Model

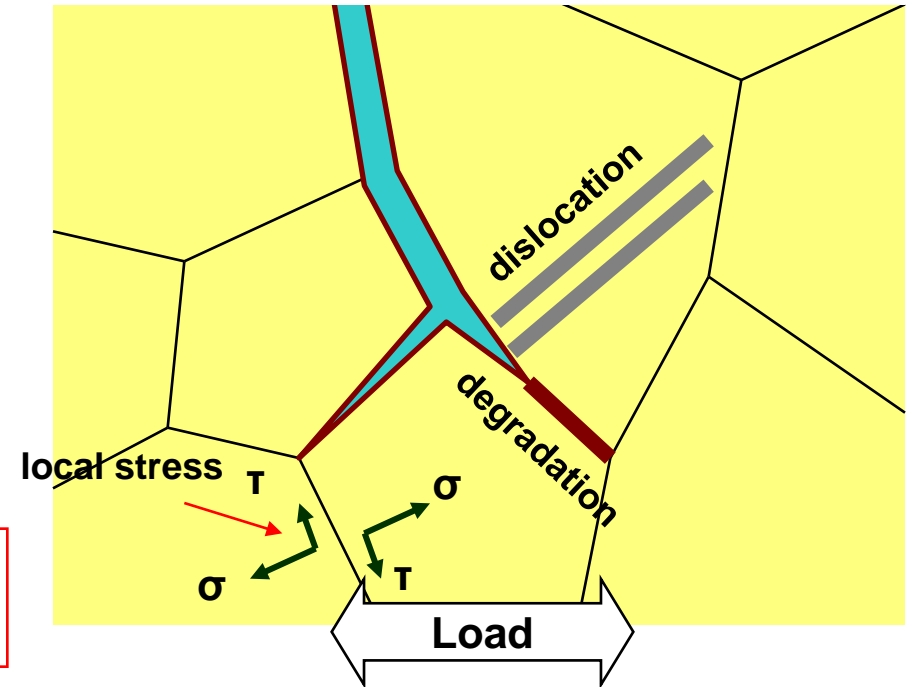
1) Setting on the strength of grain boundary

Strength of grain boundary is different by kinds of grain boundary, dislocation, ...

↔ Face centered cubic (FCC) structure has many slip planes



variations of strength of grain boundary would become small due to slip dislocation.



The strength of grain boundary with small fluctuation s_{th} is defined

$$s_{th} = s_0 + fl$$

s_0 : base strength of grain boundary
 fl : fluctuation using **normal distribution function**

2-Dimensional SCC Crack Growth Model

2) Influence of shear stress

... Complex stress constructed by vertical and shear stress is “*locally*” acted on the grain boundary around crack tip

“Net stress” h is defined

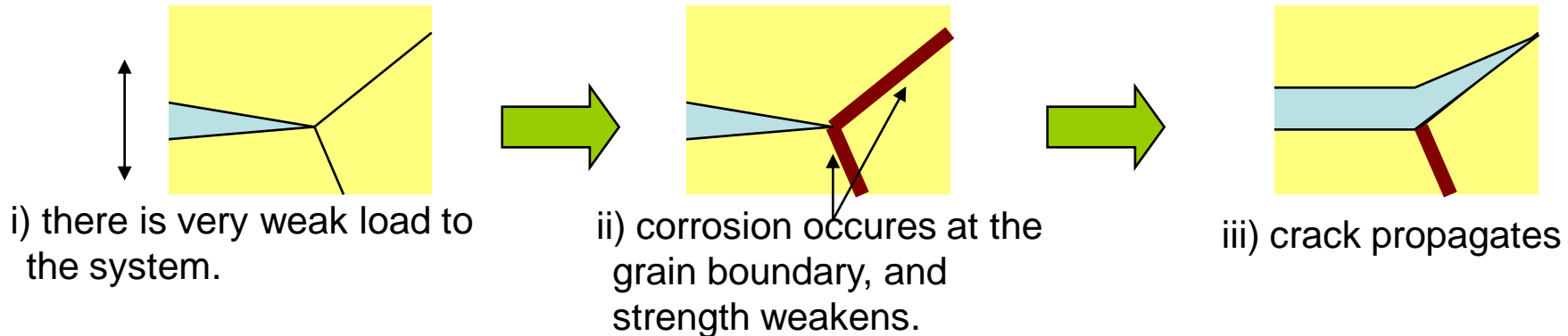
$$h = s + at$$

s : vertical stress against grain boundary
 t : shear stress against grain boundary
 a : parameter to control the effect of shear stress

3) Degradation of grain boundary

Assumption :

When the stress that acts on the grain boundary is very weak, the influence of **corrosion** is dominant relatively to that of stress factor on fracture process.



Corrosion is modeled by introducing the “**slow fracture**” of grain boundary.

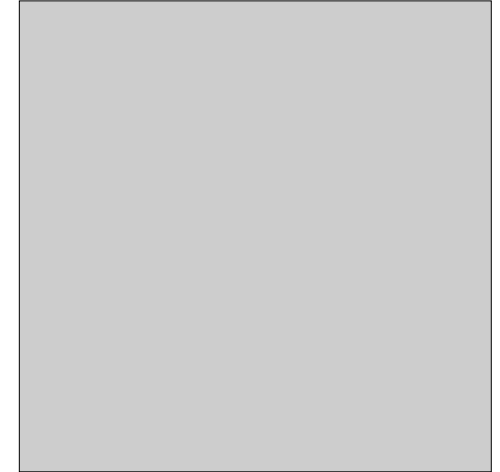
Analytical Equation of Stress at Grain Boundary

- **Vertical and shear stress around crack tip**

[Mode I]

$$s_I(r, q) = \frac{K_I}{4\sqrt{2\rho}} r^{-1/2} \frac{\sigma}{E} \left[3 \cos \frac{q}{2} + \cos \frac{3q}{2} \right]$$

$$t_I(r, q) = \frac{K_I}{4\sqrt{2\rho}} r^{-1/2} \frac{\sigma}{E} \left[\sin \frac{q}{2} + \sin \frac{3q}{2} \right]$$



Analytical Equation of Stress at Grain Boundary

K_I and K_{II} are obtained “*roughly*” using the analytical equations of stress intensity factor for the microcrack in infinite parallel-plate

$$K_I = s_0 \sin^2 f \times \sqrt{\rho a}$$

$$K_{II} = s_0 \sin f \cos f \times \sqrt{\rho a}$$

$$\left\{ \begin{array}{l} s_0 : \text{tensile stress} \\ a : \text{half length of microcrack} \\ f : \text{angle from the direction of microcrack to that of tensile stress} \end{array} \right.$$



In the model, stress dispersion by crack branching is considered.

$$k = \frac{K}{\sqrt{n}} \quad \left\{ \begin{array}{l} K : \text{stress intensity factor for no branching crack} \\ k : \text{stress intensity factor for branching crack} \\ n : \text{number of crack branching} \end{array} \right.$$

The stress around the crack tip in the model is defined as

$$\begin{aligned} s(r, f) &= s_I(r, f) + s_{II}(r, f) \\ t(r, f) &= t_I(r, f) + t_{II}(r, f) \end{aligned}$$

Flow of the Simulation

- (1) setting the system with grains, strength of grain boundary s_{th} , and initial crack
- (2) calculating number of crack branching n
- (3) calculating net stress h at the grain boundaries touched to the crack tips, and selecting largest h .

If $h > s_{th}$,

effect of stress is dominant

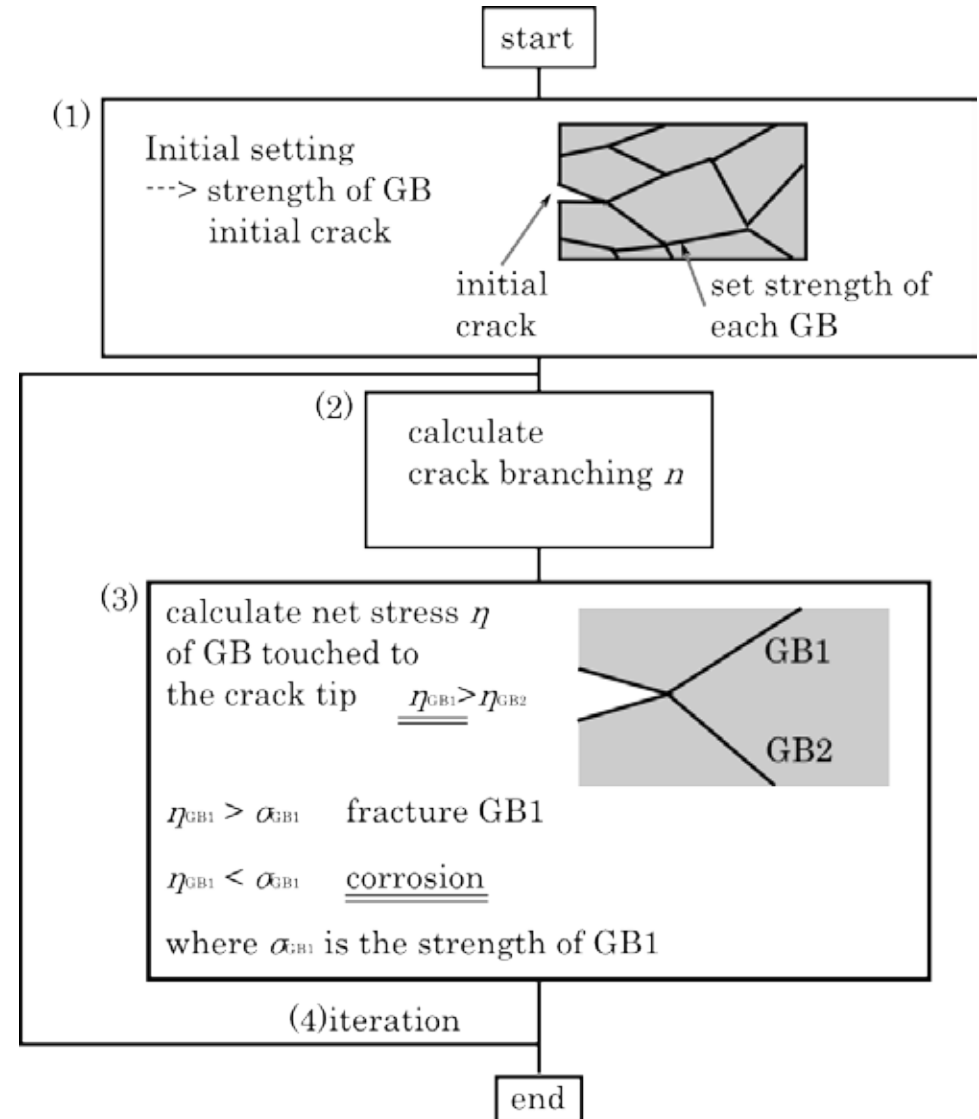
à **quick fracture**

If $h < s_{th}$,

effect of corrosion is dominant

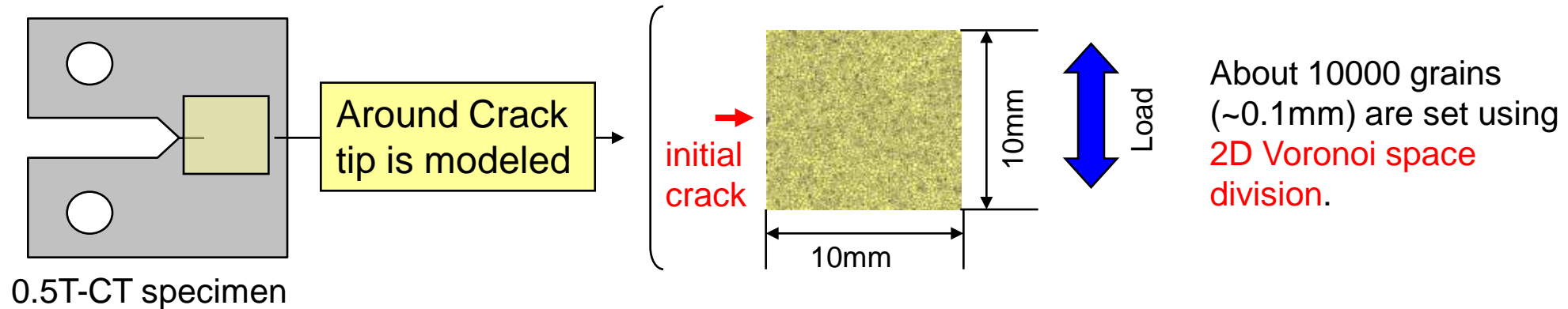
à **slow fracture**

- (4) If not final step, return to (2)



Type304 Stainless Steel IGSCC Growth Analyses

[Example] IGSCC analyses of type304 stainless steel at 400



•strength of grain boundary

base strength is set to **half of yield stress**

à 60MPa + 10% fluctuation

Assumption:

grain boundary is fractured when the half of yield stress of the applied material locally acts on the grain boundary

•Load condition

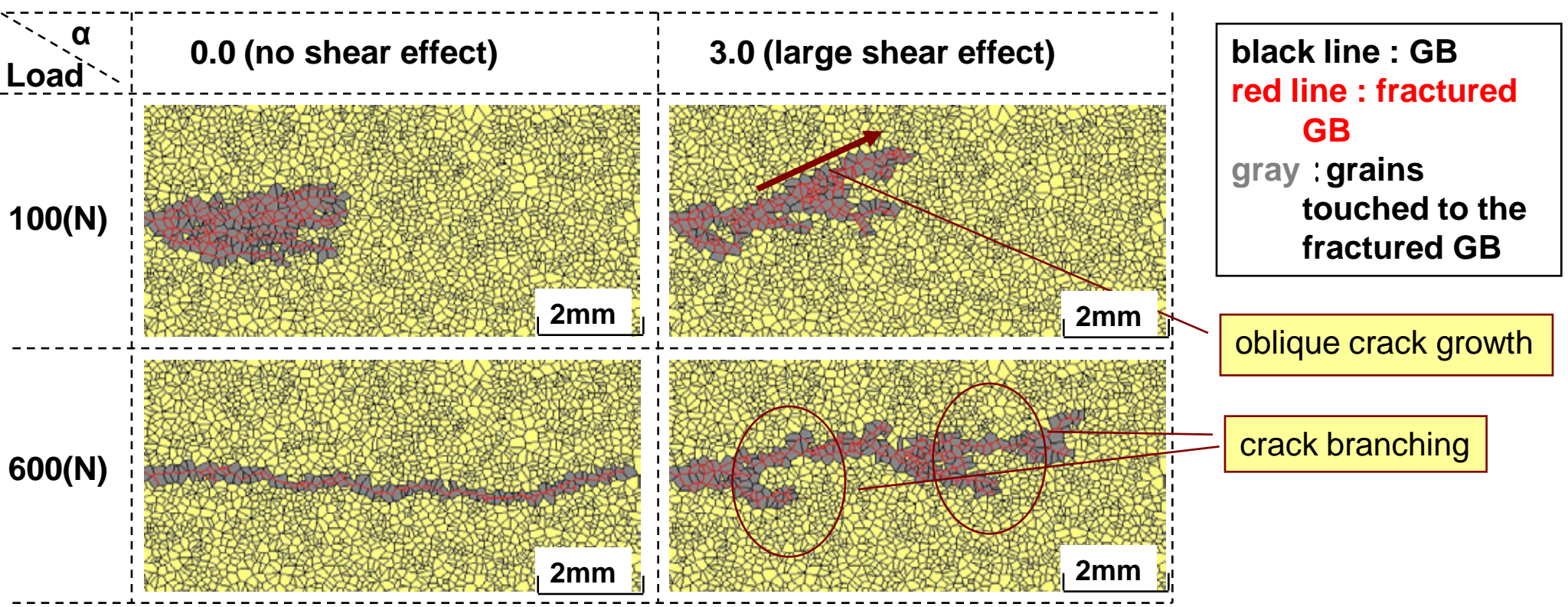
- 100 (N) : influence of corrosion is dominant
- 600 (N) : influence of stress is dominant

•parameter to controll the effect of shear stress

- 0.0 : no shear effect
- 3.0 : large shear effect

•corrosion Grain boundary fractures after 3 simulation step (fixed)

Type304 Stainless Steel IGSCC Growth Analyses: results



• 600(N), $\alpha=3.0$: **crack branching**

à The main factor of crack branching is the effect of **shear stress**

• 100(N), $\alpha=3.0$: **oblique crack growth**

à **Synergistic effect** of shear stress and corrosion of grain boundary leads to crack growth to oblique direction.

Summary

- **Development of New IGSCC Crack Growth Model**

3 kinds of characteristic effects were introduced into the model



Strength of grain boundary, Influence of shear stress,
and degradation of grain boundary

- **Type304 Stainless Steel IGSCC Crack Growth Analyses**

Using developed model, type304 stainless steel at 400 has been analyzed.

à Determine **cause of IGSCC behavior**

- (1) The main factor of crack branching is the **shear stress effect**.
- (2) The crack growth to oblique direction occurs by the **synergistic effect** of shear stress and corrosion of grain boundary.

- **Future Plans**

1. IGSCC simulation in BWR condition
2. Refinement of the effect of corrosion behavior in the model
3. Extension the model to 3-Dimensional model
4. Combination the model with Finite Element Method